## Functionally Divided Manipulation Synergy for Controlling Multi-fingered Hands

Kazuki Higashi<sup>1\*</sup>, Keisuke Koyama<sup>1</sup>, Ryuta Ozawa<sup>2</sup>, Kazuyuki Nagata<sup>3</sup>, Weiwei Wan<sup>1,3</sup> and Kensuke Harada<sup>1,3</sup>

Abstract-Synergy provides a practical approach for expressing various postures of a multi-fingered hand. However, a conventional synergy defined for reproducing grasping postures cannot perform in-hand manipulation, e.g., tasks that involve simultaneously grasping and manipulating an object. Locking the position of particular fingers of a multi-fingered hand is essential for in-hand manipulation tasks either to hold an object or to fix unnecessary fingers. When using conventional synergy based control to manipulate an object, which requires locking some fingers, the coordination of joints is heavily restricted, decreasing the dexterity of the hand. We propose a *functionally* divided manipulation synergy (FDMS) method, which provides a synergy-based control to achieves both dimensionality reduction and in-hand manipulation. In FDMS, first, we define the function of each finger of the hand as either "manipulation" or "fixed." Then, we apply synergy control only to the fingers having the manipulation function, so that dexterous manipulations can be realized with a few control inputs. Furthermore, we propose the Synergy Switching Framework as a method for applying a finely defined FDMS to sequential task changes. The effectiveness of our method is experimentally verified.

#### I. INTRODUCTION

Synergy provides a method to simultaneously control multiple Degrees of Freedom (DoFs) of a multi-fingered hand to produce coordinated movements from a limited set of input signals. One of the common strategies for controlling multi-fingered hands is to adopt synergy for their control inputs [1], [2], [3], [4], [5], [6], [7], [8], [9], [10], [11], [12], [13], [14]. For grasping an object, a synergy, hereafter called grasp synergy, can be constructed by applying the principal component analysis (PCA) to the human's hand grasping postures. The grasp synergy is then used to express various grasp postures with the multi-fingered hand using a few principal components [15], [16], [17].

The main purpose of a multi-fingered hand is to manipulate objects, including the use of tools. Using conventional synergy-based control, object grasping [12] and simple inhand manipulation (changing the pose of an object) [1] have been realized. Nevertheless, it is very challenging to achieve the required posture expressions for using human tools with the framework of conventional synergy-based

<sup>1</sup>Graduate School of Engineering Science, Osaka University; 1-3 Machikaneyama- cho, Toyonaka, Osaka 560-8531, JAPAN



Fig. 1. Overview of our proposed method. FDMS control method consists of the differentiation of the function of each finger of the hand; the ones needed for manipulation and the ones that do not need to be moved (fixed).

control. Therefore, we focus on the manipulation of human tools with a new synergy-based control method.

It is important to consider the role of each finger while manipulating tools with a multi-fingered hand. Michelman et al. [18] proposed a task partitioning method that assigns a different function to each finger of the hand and then applies a different control mode to each function. Similarly, Nagata et al. [19], [20] proposed a control system for multifingered hands in which a task containing multiple objectives is divided into functional units of the fingers. However, these conventional methods cannot solve the complexity of multifingered hand control due to its high DoFs. In this study, we propose a method to achieve both low DoFs control and dexterous manipulation by using synergy control for each function. The necessary functions and synergies are determined by considering the human motion analysis of Kamakura et al. [21].

The grasp synergy-based control assumes the coordination of all joints of a multi-fingered hand to express humanlike grasping postures. Thus, fixing the position of specific fingers heavily limits the control space of the grasp synergy. The precise posture expression, with reduced dimensionality, required for object manipulation is difficult to realize by using conventional grasp synergy-based control.

Considering the above mentioned problem, this paper proposes a *Functionally Divided Manipulation Synergy* (FDMS) method, which provides a synergy-based control for a multi-

 $<sup>\</sup>ast This$  work was supported in part by the NACHI-FUJIKOSHI Corporation.

<sup>&</sup>lt;sup>2</sup>School of Science and Technology, Meiji University

<sup>&</sup>lt;sup>3</sup>National Institute of Advanced Industrial Science and Technology

<sup>\*</sup> Corresponding author e-mail:

higashi[at]hlab.sys.es.osaka-u.ac.jp

fingered hand when manipulating an object, in which some of the fingers are used to manipulate the object while the others, which are not involve in the manipulation, are fixed in place. Figure 1 shows an overview of the proposed FDMS. Said figure shows an example of clicking downward on the top of a pen with one's thumb. In this example, the position of the remaining fingers, index, middle, ring, and little fingers are kept fixed to maintain the grasp of the pen, since they are not involve in the manipulation. First, various grasping postures of a human hand are measured in advance. Then, we construct FDMSs based on the principal component vectors of the measured human hand's postures including only the fingers or joints needed for the manipulation.

Similarly, we consider the situation where a robot first picks a pen and then press the top of the pen. The robot first grasps the pen by using the grasp synergy based control, then uses the FDMS method to control only the thumb to click downward the top of the pen while the other fingers are used to maintain a grasp of the pen. In said case, we switch among multiple FDMSs and fix different fingers according to the task. Therefore, we propose a framework named Switching Synergy Framework. The Switching Synergy Framework makes the FDMSs useful to perform various sequential tasks.

The main contribution of our work the realization of inhand manipulation task with few-dimensional control inputs by using the FDMS method and the Switching Synergy Framework. FDMS is constructed for each function of fingers so that the control space is not constrained by fixing some specific fingers. The number of FDMSs needed can be defined by using the Kamakura's notation [21]. Furthermore, it is shown that the Synergy Switching Framework scales to the real environment where the task is in transition.

This paper is organized as follows. The related work on the synergy and multi-fingered hands are introduced in Section II. Our proposed method using FDMS is depicted in Section III and Section IV. Our proposed Switching Synergy Framework which makes FDMS useful to apply in sequential tasks is described in Section V. Section VI describes the experiments conducted to evaluate the proposed methods. The results and comparisons between methods are described in Section VII.

#### II. RELATED WORK

The concept of synergy has drawn attention in the robotics research community. Synergy provides an effective method for controlling multi-fingered hands with few dimensional control inputs. Santello et al. [15] measured human hand motions during daily life, assuming a 15 DoFs kinematics model and showed that 80% of the movements could be realized with just two principal components. Similarly, Todorov et al. [22] showed that four principal components represent 85% of the movements when assuming a 20 DoFs kinematics model. Xiong et al. [6] developed a synergy-based multi-fingered hand that can realize 30 kinds of grasping poses out of 33 poses defined by Feix [23]. Chen et al. [24] developed a synergy-based hand based on the 2 DoFs angular velocity synergy, implemented by using cam and underactuated mechanism.

Although grasp synergy provides an effective method for controlling multi-fingered hands, the research on performing tasks with synergy-based control is limited.

Kent et al. [8] proposed the task dependent temporally synchronized synergies (TSS) for performing a task by using a prosthetic hand according to the EMG signal of a human. TSS is an attractive method that enables us to generate dexterous motion of an object, but to create a TSS, humans need to measure the motion for each task. In general, a multifingered hand is required in a large number of tasks, so the TSS method has a very high measurement cost. Our method, FDMS, is constructed from a variety of grasping postures, similar to grasp synergies. Thus, the measurement cost is low, and it is only necessary to assign specific functions to each finger to perform tasks.

Santina et al. [1] developed a synergy-based multi-fingered hand and demonstrated the effectiveness of the adaptive synergy [2] through some complex tasks such as grasping and opening a screw cap. However, the conventional grasp synergy-based control is not suitable for performing dexterous manipulation tasks that involve grasping and manipulating an object simultaneously. This is because if we try to fix the position of a finger of the multi-fingered hand when performing a task, the control space spanned by its principal component vectors is heavily restricted and cannot express the postures required for the dexterous manipulation tasks.

On the other hand, our proposed synergy-based control can perform dexterous tasks such as manipulating an object while grasping that without being affected by fixed fingers because for constructing the synergy we only consider the fingers involved in the manipulating function.

Michelman et al. [18] proposed a method of assigning functions to each finger and then applying a control mode per function to perform a specific task. They realized inhand manipulation while controlling the force applied to an object with a three-fingered robotic hand. In this study, we apply FDMS, a finger-level synergy control, to the task partitioning proposed by Michelman et al. to achieve in-hand manipulation in low dimensions.

#### III. SYNERGY

#### A. synergy control

Synergy, in the context of control of a multi-fingered hand, is defined to be the coordination of joints and defines the basis of the joint-angle space. In this section, we first formulate synergy introduced in this research.

By using a set of hand poses, the posture sequence X used for formulating synergy can be defined as:

$$\boldsymbol{X} = [\boldsymbol{p}_1, \boldsymbol{p}_2, \cdots, \boldsymbol{p}_j, \cdots, \boldsymbol{p}_n]^T, \qquad (1)$$

where  $p_i$   $(i = 1, \dots, n)$  denotes a *d*-dimensional vector expressing a configuration of a multi-fingered hand. We assume that each pose included in **X** is sufficiently diverse to cover most human grasping postures.

In this research, we make a multi-fingered hand manipulating an object by using some of the fingers while others are used to grasp or simply fixed. We formulate such division of the finger functions. By defining the indices of all joints included in the hand as  $J = \{1, 2, ..., d\}$ , we can define the subset of f joints from J as  $J^{\text{sub}} = \{s_1, \dots, s_j, \dots, s_f\} \subseteq J$ where  $J^{\text{sub}}$  is defined to be a set of joints included in some of the fingers to realize a specific function. By using  $J^{\text{sub}}$ , a hand pose  $\boldsymbol{p}_j^{\text{sub}}$  can be represented as:

$$\boldsymbol{p}_{i}^{\text{sub}} = [p_{i,s_{1}}, p_{i,s_{2}}, \cdots, p_{i,s_{j}}, \cdots, p_{i,s_{f}}]^{T}$$
(2)

From (2), we can obtain the posture sequence  $\mathbf{X}^{\text{sub}}$  consisting of  $\mathbf{p}_i^{\text{sub}}, i = 1, \dots, n$ . The principal component analysis (PCA) of the extracted hand pose is equivalent to the eigenvalue problem for its covariance matrix. The eigenvectors  $\mathbf{a}_1, \dots, \mathbf{a}_f$  and the eigenvalues  $\lambda_1, \dots, \lambda_f$  represent the coordination of joints and the variance of each principal component, respectively. Finally, we can define a synergy matrix *S* for the  $n_s$ -dimensional synergy control as follows:

$$S = [\boldsymbol{a}_1, \cdots, \boldsymbol{a}_{n_s}] \tag{3}$$

#### B. synergy definition

Now we define three different synergies, the most commonly used, grasp synergy, the functionally divided manipulation synergy proposed in this paper and the task-specific synergy.

We first introduce the grasp synergy which is equivalent to the conventional definition of synergy:

Definition 1: Grasp Synergy is defined to be a synergy composed of various grasping postures in X. Grasp synergy considers the total joint space J of a human hand or a multi-fingered hand.

On the other hand, we aim to make a multi-fingered hand to perform a task. We introduce the following two definitions of synergy for performing a task. Among the two definitions, the Functionally Divided Manipulation Synergy (FDMS) proposed in this paper will be defined later in the next section. For the comparison study, we introduce synergy for performing a specific task:

*Definition 2:* **Task-Specific Synergy** of the *k*-th task is defined to be a synergy composed of hand postures  $\boldsymbol{X}_{k}^{T}$  performing the *k*-th task considering the total joint space J of a human hand or a multi-fingered hand. The synergy matrix of the *k*-th task-specific synergy is denoted as  $S_{k}^{T}$ .

#### C. postures approximation

In synergy-based control, it is important to evaluate how precisely a hand posture can be realized for performing a required task. To evaluate the capability to express such function-required postures, we verify whether or not a task succeeds when hand postures are presented in the synergy space. By using the synergy matrix, an approximated posture  $\hat{p}$  is given by:

$$\hat{\boldsymbol{p}} = SS^T \boldsymbol{p},\tag{4}$$

where  $SS^T$  denotes an orthogonal projection matrix projecting a joint angle vector to the synergy space. This accuracy of approximated posture is used to evaluate each synergy. The posture sequence  $\hat{X}$  approximated by a synergy can be expressed by:

$$\hat{\boldsymbol{X}}^{T} = SS^{T}\boldsymbol{X}^{T} = [\hat{\boldsymbol{p}}_{1}, \hat{\boldsymbol{p}}_{2}, \cdots, \hat{\boldsymbol{p}}_{j}, \cdots, \hat{\boldsymbol{p}}_{N}]$$
(5)

# IV. FUNCTIONALLY DIVIDED MANIPULATION SYNERGY (FDMS)

In this section, we further formulate the FDMS method based on the typical movement units of human hands. We assign two kinds of functions (Manipulating and Fixed) to each finger based on a study of finger motion analysis for manipulating an object [21]. We also identify necessary FDMSs based on typical finger movements and their frequency.

#### A. Typical unit movements of human hands

To analyze the human hand motion, we introduce the Kamakura's XYZ-notation, which defines the finger movement when manipulating an object [21]. The XYZ-notation method decomposes a series of human hand motions, manipulating an object, into movement units. The movement unit for a given manipulation task is defined with respect to the movement of each finger, considering them in sequential order from the thumb to the little finger. Each finger is assigned a symbol X, Y, Z, or O according to the following conditions. Kamakura defined discretized cluster of a finger movement. If a finger movement is categorized into the same cluster, we assign the same symbol. Firstly, if there is any movement of the thumb, assign the symbol X. Next, if the movement of the index finger is the same as the movement of the thumb, assign the same symbol X. If the movement is different, assign the symbol Y. Similarly, if the movement of the middle finger is the same as the thumb, assign the symbol X, if different from the thumb but the same as the index finger, assign the symbol Y. Moreover, if the movement of the middle finger is different from both the thumb and the index finger, assign it the symbol Z. The symbol Ois assigned to a finger that has no motion during a given manipulation task. According to [21], for most of the daily tasks, each finger performs at most three different motions. This is because only XYZ are used to express finger motion. According to the XYZ-notation, the movement of a human hand can be described with five characters. An example of using the XYZ-notation to characterize a task is shown in Figure 2. In said example, the task of manipulating a pen is considered as being composed of four phases; grasping the pen, preparing grasping posture for clicking the top of the pen, preparing posture of the thumb, and then clicking downward the top of the pen, to expose the ballpoint.

Table I shows the typical unit movements and their frequency obtained from the analysis of human motions manipulating an object [21]. Said table lists all the unit movements whose frequency exceeds 1%. More than 68.4% of unit movements can be expressed by using the mentioned four symbols of the XYZ-notation. In addition, the frequency



Fig. 2. Appearance of a pen-knocking task. (Phases): describes the purpose of each unit movement. (Motion of each finger): shows the kind of finger motion and the relation between motion of each finger. (Images): depicts each phase of the task. (XYZ-notation): shows the notation of each movement by using XYZ-notation described in Section IV-A. (FDMS): shows what kind of FDMS defined in Section IV-B use for the movement

 TABLE I

 Typical movement unit and its frequency[21]

Movement unit	Frequency[%]
XXXXX	8.5
XYYYY	9.0
X0000	8.9
OXXXX	3.5
XXYYY	1.9
XX000	3.2
OOXXX	5.1
OOOXX	2.4
XYZZZ	3.5
XYOOO	4.8
OXYYY	2.6
0X000	8.9
XYYOO	1.9
00X00	1.9
OOXXO	1.3
XYYYO	1.0
Total	68.4

of unit movements in a state where at least one finger does not move is 45.5%, implying that it is necessary to fix particular fingers when manipulation an object with human hands.

#### B. Necessary FDMSs

As mentioned above, the XYZ-notation method decomposes a series of human-hand motions into movement units. However, each symbol in the XYZ-notation does not explain what function each finger has. In this study, we define the following two symbols to describe the function of each finger, in relation to the XYZ-notation.

1) Manipulation : M

is assigned to the fingers required for manipulating an object. This corresponds to X, Y, and Z in the XYZ-notation.

2) Fixed : F

is assigned to a finger that needs to be fixed with its current posture, either because it is necessary to keep that posture (e.g. to maintain a grasping posture), or

 TABLE II

 UNITS OF FDMS (M: A FINGER INCLUDED IN FDMS CONSTRUCTION)

Joint Subspace	FDMS Units
$J_1^{ m sub}$	MMMMM
$J_2^{ m sub}$	MFFFF
$J_3^{sub}$	FMMMM
$J_4^{sub}$	MMFFF
$J_5^{sub}$	FFMMM
$J_6^{sub}$	FFFMM
$J_7^{sub}$	FMFFF
$J_8^{sub}$	MMMFF
$J_9^{sub}$	FFMFF
$J_{10}^{sub}$	FFMMF
$J_{11}^{sub}$	MMMMF
J <sup>sub</sup> <sub>12</sub>	FMMMF

because the finger is not necessary for the task. This corresponds to  $\circ$  in the XYZ-notation.

To avoid assigning multiple manipulating functions to different fingers within a single movement unit, we divide the movement unit into several units to include only a single manipulating function per movement unit. For example, when we use the computer mouse with a unit movement OXYOO, the index finger is assigned the function of left-clicking and the middle finger is assigned the function of right-clicking. In said case, we divide the movement unit into two units as  $OXYOO \rightarrow OXOOO + OOXOO$ . We applied the same operation to all movement units in the Table I. The resulting movement units are shown in Table II.

Finally, we can define 12 joint subspaces  $J_l^{\text{sub}}(l = 1, \dots, 12)$  of FDMS consisting of only fingers assigned M in Table II. Base on these joint subspaces, we define the FDMS as follows:

Definition 3: Functionally Divided Manipulation Synergy (FDMS) is defined to be a synergy composed of various grasp postures  $X^g$  considering *l*-th joint subspace  $J_l^{\text{sub}}$  of a human hand or a multi-fingered hand. The synergy matrix of the FDMS is denoted as  $S_l^f$ .

FDMS are constructed in a similar fashion as grasp synergies. Therefore, the FDMS consisting of all joint subspaces



Fig. 3. The overview of Switching Synergy Framework. In this research, FDMSs are registered in a synergy database, and the synergies are changed according to the change of functions.

is equivalent to the grasp synergy.

#### V. SWITCHING SYNERGY FRAMEWORK

When performing a task, the function required for a finger changes according to the situation. Hence, it is necessary to switch among multiple FDMS according to the change of functions. In this research, we propose Synergy Switching Framework as a framework for switching synergies. Figure 3 depicts the overview of the Synergy Switching Framework. Within the said framework, several synergies that can perform various tasks are prepared in advance and a synergy database is constructed. The user inputs the task to be performed into the system and selects a synergy suitable for performing the task. Depending on the characteristics of the synergies registered in the synergy database, the granularity of the task division and the required inputs vary. In this study, we register 12 FDMSs defined in Section IV-B to the synergy database.

#### VI. EXPERIMENTAL ENVIRONMENT

#### A. Human's Hand Pose Measurement

To measure the posture of the human hand, we use CyberGlove III [25]. The CyberGlove III can measure the joint angles of the human hand at 100Hz. In this study, only the motion of fingers was considered, without considering the motion of the wrist. Therefore, the angles of 20 joints were measured.

#### B. Teleoperating System

The teleoperating system consists of a UR3e robotic arm, a 10 DoFs humanoid hand, and a CyberGlove III. The subject equipped with the CyberGlove III performs a task by transferring postures to the 10 DoFs humanoid hand. The movement of the UR3e robotic arm was controlled through keyboard inputs.

#### C. Tasks

In order to evaluate the performance of our method, FDMS, two tasks were conducted: an opening/closing task of scissors and a pushing task of a switch. These tasks



Fig. 4. Overview of experimental setup. Teleoperating a 10 DoFs Humanoid Hand using a CyberGlove Ⅲ

utilize tools that have not been thoroughly considered in previous research. In addition, the tasks of using scissors and pressing a switch were selected as a representative example of tasks that required both to grasp and manipulate at the same time. Following the notation described in Section IV-B, the mentioned tasks are considered as follows: when using scissors, the thumb, index, and middle finger are thought to have a Manipulation function. For pushing the switch, at first, all fingers are assigned the Manipulation function. Then, only the thumb is assigned with the Manipulation function while the other fingers are assigned the Fixed function.

The overall experimental setup for the tasks described above is shown in Figure 4. In both cases, first, the target object is grasped from a fixed initial position on the table. The first task is considered completed if fingers of a humanoid hand inserted into the scissors, and then the scissors were opened/closed three times. Similarly, for the second task, it is considered successful if the switch was fully pressed.

The human operator performed each task for 20 times and measured postures sequences of the hand with the Cyber-Glove III. For each task, 10 postures sequences  $\boldsymbol{X}_k^T$  were used to construct the task-specific synergy and the remaining 10 sequences  $\boldsymbol{X}_m^E(m = 1 \cdots 10)$  are used for evaluation.

#### D. Synergies

We first constructed the grasp synergy from principal components of a variety of grasping postures. The major 33 grasping postures of a human were used based on the grasp taxonomy proposed in [23]. The humanoid hand postures are measured while the fingers are moved from a parallel and flatten posture to the target grasping posture. Then, the posture sequence  $X^g$  was constructed, as mentioned in Section III-B, with postures excluding the overlapping postures. Subsequently, the grasp synergy  $S^g$  has been constructed based on the grasp posture sequence  $X^g$ .

For comparative evaluation, the *task-specific synergy* was introduced. The task-specific synergy was made of multi-fingered hand postures extracted while performing each specific task, e.g., opening/closing a scissors and pressing a switch, independently. The hand poses were extracted by

### TABLE III

THE FUNCTIONS OF EACH FINGER WHEN PERFORMING THE SCISSORS-TASK AND THE SWITCH-TASK.

Loint	Function		
Joint	Scissors-task	Switch-task	
Thumb rot.	М	М	
Thumb MCP	М	М	
Index MCP	М	F	
Index PIP	М	F	
Middle MCP	М	F	
Middle PIP	М	F	
Ring MCP	F	F	
Ring PIP	F	F	
Pinky MCP	F	F	
Pinky PIP	F	F	

teleoperating the 10 DoFs humanoid hand. In each case, the task was performed ten times. Then, the *task-specific synergies* were created by principal component analysis as  $S_{scissors}^{T}$  and  $S_{switch}^{T}$ .

We consider each task as having two phases, a grasping phase, and a manipulation phase. For the grasping phase, the grasp synergy-based control method is used. For the manipulation phase, the proposed FDMS-based control method is used. To construct FDMS, it is necessary to define the function of the fingers for each task, scissors-task, and switch-task. Table III shows the defined function of each finger when performing the scissors-task and the switchtask. These functions are empirically defined. The functions are assigned according to Section IV-B. The set consists of joint assigned M, and defined as  $J^{sub}$ . We construct FDMS by using  $J^{\text{sub}}$  according to Section III-B. Note that the maximum number of principal components is the number of joints assigned M. The switch-task has two phases: the grasping phase and the manipulation phase. Therefore, we switch synergies according to the Switching Synergy Framework, from grasp synergy to FDMS.

#### E. Evaluation

1) The task success rate: In this experiment, we examined how many dimensions are reduced when using each synergy-based control method to perform the tasks in the real environment. The performance of conventional synergies was evaluated mainly by the contribution ratio which is percent variance accounted for by a principal component. However, it has not been verified whether tasks can be performed by using a synergy with a high contribution ratio. To evaluate performance, we focus on the task success rate when replaying the posture sequences  $\mathbf{X}_m^E(m = 1 \cdots 10)$ approximated by the synergy according to Section III-C on the teleoperating system. The task success rate is calculated based on the percentage of successful tasks played by the approximated posture sequence.

2) Practical demonstration: We considered two more challenging tasks, a Cutting-task and a Spray-task. In the Cutting-task, the scissors placed on the workspace in advance are grasped, and a string is cut by operating the scissors. Similarly, in the Spray-task, the hand grasps and manipulates



Fig. 5. **Scissors-task**: Relation between the number of principal components and success rates. The maximum number of principal components of FDMS for the scissors-task is 6 since the FDMS is composed 6 DoFs joint subspace.



Fig. 6. **Switch-task**: Relation between the number of principal components and the success rates. Switch-task includes the change of synergy from grasp synergy to FDMS according to the Switching Synergy Framework since the fingers' function changes during the task. The blue and green lines show the success rate when the number of principal components of grasp synergy changes and we fix the number of principal components of the FDMS to 1 and 2 respectively.

a spray bottle placed on the workspace by pulling the lever. We evaluate whether the Cutting-task and Spray-task can be realized, as more practical tasks. In this experiment, the trajectory of the hand is generated by our teleoperation system, but note that the posture obtained from CyberGloveI II is approximated by our FDMS method in real-time. The pose of the object is known, and the movement of the arm is also determined in advance.

#### VII. RESULTS

For each task, we show the plot of the success rate as a function of the number of principal components in Figure 5 (scissors-task) and Figure 6 (switch-task). Both results show that, as the number of principal components increases, the task success rate increases. Regardless of the number of principal components, the success rate of using FDMS is higher than the success rate of using conventional grasp synergy.

In the scissors-task, Figure 5, the highest success rate when using the conventional grasp synergy is 70%. In contrast, using our FDMS with four principal components achieved a task success rate of 90%. By fixing the position of some fingers, which are not necessary for the task, we reduce the overall DoF. Thus the accuracy of posture expression of FDMS improves due to the mathematical properties of PCA. On the contrary, if the position of those fingers is not fixed, then they may interfere with the manipulated object.

On the other hand, task-specific synergy achieved a task success rate of almost 100% regardless of the number of principal components used. Therefore, when the number of tasks required for a humanoid hand is small, the said result implies that a high task success rate can be achieved by switching task-specific synergies according to the Switching Synergy Framework.

In the switch-task, Figure 6, when using the FDMS with just a single principal component, the task success rate is always 0 since the fingers whose function is the manipulating do not work well. This result shows that the thumb of the multi-fingered hand needs at least two DoFs. When using the grasp synergy with two principal components and the FDMS with two principal components, a task success rate of 90% is achieved. In this case, the dimensions of the control space of the grasp synergy and the FDMS are always two, so it can be said that the effect of dimensionality reduction has been fully demonstrated.

#### VIII. DISCUSSION

As shown in Figure 5 and Figure 6, to achieve the task success rate of 100% using the task-specific synergy, the scissors-task requires only one principal component, while the switch-task requires at least four principal components. The reason is that, in the switch-task, the fingers assigned for manipulating function changes from the index, middle, ring, and pinky fingers to the only thumb according to the transition of the task. Since the task-specific synergy assumes the coordination of all fingers, it usually cannot perform multiple functions. This result suggests that the Switching Synergy Framework, which can switch FDMS, is effective for tasks that are required to change the fingers' function.

Figure 7 shows the hand performing the Cutting-task and Spray-task when using FDMS-based control and the Switching Synergy Framework. In the Cutting-task, the hand can grasp the scissors and cut the string by using only two principal components for the FDMS. In the spray-task, the hand has to grasp with all fingers and then push its lever with only the index finger while the other fingers maintain the grasping state. Maintaining the grasp state is essential for manipulating the lever, this fact confirms the importance of fixing some of the fingers. Thus, the grasp synergy-based control with a few principal components cannot realize the spray-task. In contrast, FDMS and the Switching Synergy Framework can realize the spray-task by using 2 DoFs grasp synergy and 1 DoF FDMS. These facts suggest that FDMS and Switching Synergy Framework effectively supply the control spaces spanned by a few principal components, which can realize various sequential tasks.

The conventional grasp synergy can generate trajectories to grasp objects [12] and perform in-hand manipulation





Fig. 7. Demonstration of the cutting-task and the spray-task using FDMSbased control and the Switching Synergy Framework

such as changing the pose of an object [1]. Therefore, it is considered that FDMS, which is a form of grasp synergy limited by joint subspace, can generate the trajectory for grasping and manipulation.

In this study, we empirically determine the fingers' functions and its change during each task. However, in order to use FDMS and Switching Synergy Framework in a real environment, the functions required for a task should be automatically determined and assigned to the finger. In this study, it was possible to limit the number of FDMS required for manipulating an object to 12. Interesting future research would be to construct a Markov process with these 12 FDMSs as states. It is possible to construct a system that selects an appropriate FDMS from observations of the target task.

While we define just two functions to compose the FDMS, more detailed functions can be introduced to make our FDMS more useful. For instance, we can introduce a 'main-taining grasp' function derived from the fixed function to control the force applied to the grasped object. These force-centric functions make our approach more valuable and we can easily implement them by using conventional works [12], [18].

The posture expression ability required to realize a manipulating function is considered to be different for each FDMS. If we develop a multi-fingered hand that realizes FDMS, it is necessary to determine in advance how many principal components should be used for each synergy. Now, we discuss a method using a cumulative contribution ratio as one of the methods. Cumulative contribution ratio is the sum of contribution ratios from the first principal component to the *f*-th principal component in PCA and indicates how

#### TABLE IV

The number of principal components to achieve cumulative contribution ratio 80% or 90%

Joint subspace	Movement unit	Number of PCs	
Joint subspace Movement unit	>80%	>90%	
$J_1^{\text{sub}}$	MMMMM	3	4
$J_2^{sub}$	MFFFF	1	2
$J_3^{\tilde{s}ub}$	FMMMM	2	3
$J_4^{\rm sub}$	MMFFF	2	3
$J_5^{\rm sub}$	FFMMM	1	2
$J_6^{sub}$	FFFMM	1	2
$J_7^{sub}$	FMFFF	1	2
$J_8^{sub}$	MMMFF	3	4
$J_{9}^{sub}$	FFMFF	3	4
$J_{10}^{sub}$	FFMMF	1	2
$J_{11}^{sub}$	MMMMF	3	4
$J_{12}^{sub}$	FMMMF	2	3

well the variance of the samples can be explained. Therefore, if an FDMS realizes a high cumulative contribution ratio, it is considered that the FDMS has a high posture expression ability. Table IV shows the number of principal components required for each FDMS shown in Table II to achieve a cumulative contribution ratio of 80% or 90%. The FDMS is the same as the one used in the experiment, defined in Section VI-D. Note that the maximum number of principal components of each FDMS is twice the number of M from the definition and the configuration of 10 DoFs multifingered hand. The results suggest that at most three and four principal components are sufficient to achieve the cumulative contribution ratios of 80% and 90%, respectively.

#### IX. CONCLUSION

In this paper, we proposed the Functionally Divided Software Synergy method, which can realize manipulation tasks using a multi-fingered hand, with a high success rate. It was confirmed that fixing some specific fingers was important for manipulating objects. Experiments confirmed that FDMS is effective for manipulation tasks. Moreover, the required FDMS to manipulate an object can be limited to 12 based on the motion analysis of the human hand, and the cost is lower than constructing task-specific synergies, which would required the configuration of synergies for each particular task.

Future works will aim to develop the method to design an under-actuated multi-fingered hand leveraging FDMS, the system to assign functions to fingers according to information of an object, and functions that consider force between fingers and an object.

#### REFERENCES

- C. D. Santina, C. Piazza, G. Grioli, M. G. Catalano, and A. Bicchi, "Toward dexterous manipulation with augmented adaptive synergies: The pisa/iit softhand 2," *IEEE Trans. on Robotics*, pp. 1–16, 2018.
- [2] M. G. Catalano, G. Grioli, A. Serio, E. Farnioli, C. Piazza, and A. Bicchi, "Adaptive synergies for a humanoid robot hand," in 2012 12th IEEE-RAS Int. Conf. on Humanoid Robots (Humanoids 2012), 2012, pp. 7–14.
- [3] M. T. Ciocarlie and P. K. Allen, "Hand posture subspaces for dexterous robotic grasping," *The International Journal of Robotics Research*, vol. 28, no. 7, pp. 851–867, 2009.

- [4] P. Michelman and P. Allen, "Compliant manipulation with a dextrous robot hand," in [1993] Proceedings IEEE International Conference on Robotics and Automation, 1993, pp. 711–716 vol.3.
- [5] J. B. Rosmarin and H. H. Asada, "Synergistic design of a humanoid hand with hybrid dc motor - sma array actuators embedded in the palm," in 2008 IEEE Int. Conf. on Robotics and Automation, May 2008, pp. 773–778.
- [6] C. H. Xiong, W. R. Chen, B. Y. Sun, M. J. Liu, S. G. Yue, and W. B. Chen, "Design and implementation of an anthropomorphic hand for replicating human grasping functions," *IEEE Trans. on Robotics*, vol. 32, no. 3, pp. 652–671, 2016.
- [7] G. Palli, C. Melchiorri, G. Vassura, U. Scarcia, L. Moriello, G. Berselli, A. Cavallo, G. D. Maria, C. Natale, S. Pirozzi, C. May, F. Ficuciello, and B. Siciliano, "The dexmart hand: Mechatronic design and experimental evaluation of synergy-based control for human-like grasping," *The Int. J. of Robotics Research*, vol. 33, no. 5, pp. 799– 824, 2014.
- [8] B. A. Kent, J. Lavery, and E. D. Engeberg, "Anthropomorphic control of a dexterous artificial hand via task dependent temporally synchronized synergies," *J. of Bionic Engineering*, vol. 11, no. 2, pp. 236 – 248, 2014.
- [9] N. Roy, P. Newman, and S. Srinivasa, An Object-Based Approach to Map Human Hand Synergies onto Robotic Hands with Dissimilar Kinematics. MIT Press, 2013, pp. 504–.
- [10] J. Romero, T. Feix, C. H. Ek, H. Kjellstrm, and D. Kragic, "Extracting postural synergies for robotic grasping," *IEEE Trans. on Robotics*, vol. 29, no. 6, pp. 1342–1352, Dec 2013.
- [11] T. Wimbek, B. Jahn, and G. Hirzinger, "Synergy level impedance control for multifungered hands," in 2011 IEEE/RSJ Int. Conf. on Intelligent Robots and Systems, Sep. 2011, pp. 973–979.
- [12] F. Ficuciello, "Synergy-based control of underactuated anthropomorphic hands," *IEEE Trans. on Industrial Informatics*, vol. 15, no. 2, pp. 1144–1152, Feb 2019.
- [13] F. Ficuciello, D. Zaccara, and B. Siciliano, "Synergy-based policy improvement with path integrals for anthropomorphic hands," in 2016 *IEEE/RSJ Int. Conf. on Intelligent Robots and Systems (IROS)*, Oct 2016, pp. 1940–1945.
- [14] F. Ficuciello, G. Palli, C. Melchiorri, and B. Siciliano, "Postural synergies of the ub hand iv for human-like grasping," *Robotics and Autonomous Systems*, vol. 62, no. 4, pp. 515 – 527, 2014.
- [15] M. Santello, M. Flanders, and J. F. Soechting, "Postural hand synergies for tool use," *J. of Neuroscience*, vol. 18, no. 23, pp. 10105–10115, 1998.
- [16] M. Gabiccini, G. Stillfried, H. Marino, and M. Bianchi, "A data-driven kinematic model of the human hand with soft-tissue artifact compensation mechanism for grasp synergy analysis," in 2013 IEEE/RSJ Int. Conf. on Intelligent Robots and Systems, 2013, pp. 3738–3745.
- [17] J. N. Ingram, K. P. Krding, I. S. Howard, and D. M. Wolpert, "The statistics of natural hand movements," *Experimental brain research*, vol. 188, no. 2, pp. 223 – 36, 2008.
- [18] P. Michelman and P. Allen, "Forming complex dextrous manipulations from task primitives," in *Proceedings of the 1994 IEEE International Conference on Robotics and Automation*, 1994, pp. 3383–3388 vol.4.
- [19] K. Nagata and F. Saito, "Manipulation with a multi-fingered robot hand based on cooperation of finger primitive operations," in 2008 IEEE Int. Conf. on Robotics and Biomimetics, 2009, pp. 889–894.
- [20] K. Nagata and N. Yamanobe, "Picking up a towel by cooperation of functional finger actions," in 2009 IEEE/RSJ Int. Conf. on Intelligent Robots and Systems, 2009, pp. 1785–1790.
- [21] N. Kamakura, "Form of hand and motion of hand (in japanese)," Ishiyaku Publishers, 1989.
- [22] E. Todorov and Z. Ghahramani, "Analysis of the synergies underlying complex hand manipulation," in *The 26th Annual Int. Conf. of the IEEE Engineering in Medicine and Biology Society*, vol. 2, 2004, pp. 4637–4640.
- [23] T. Feix, J. Romero, H. B. Schmiedmayer, A. M. Dollar, and D. Kragic, "The grasp taxonomy of human grasp types," *IEEE Trans. on Human-Machine Systems*, vol. 46, no. 1, pp. 66–77, 2016.
- [24] W. Chen, C. Xiong, and S. Yue, "Mechanical implementation of kinematic synergy for continual grasping generation of anthropomorphic hand," *IEEE/ASME Transactions on Mechatronics*, vol. 20, no. 3, pp. 1249–1263, June 2015.
- [25] CyberGlove Systems LLC, http://www.cyberglovesystems.com/ cyberglove-iii.